# Experiment of the 200-meter DC superconducting power cable and Perspectives of DC Superconducting power transmission and distribution

# Satarou Yamaguchi

and

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- 1) Results of the 20-meter Cable Experiment
- 2) Design & Construction of the 200-meter Cable Test Facility
- 3) Results of the 200-meter Cable Experiment
- 4) Future Projects & Comments

### **20-meter Cable Experiment**

IASS Workshop @2011/05/13, Potsdam



#### Parameters

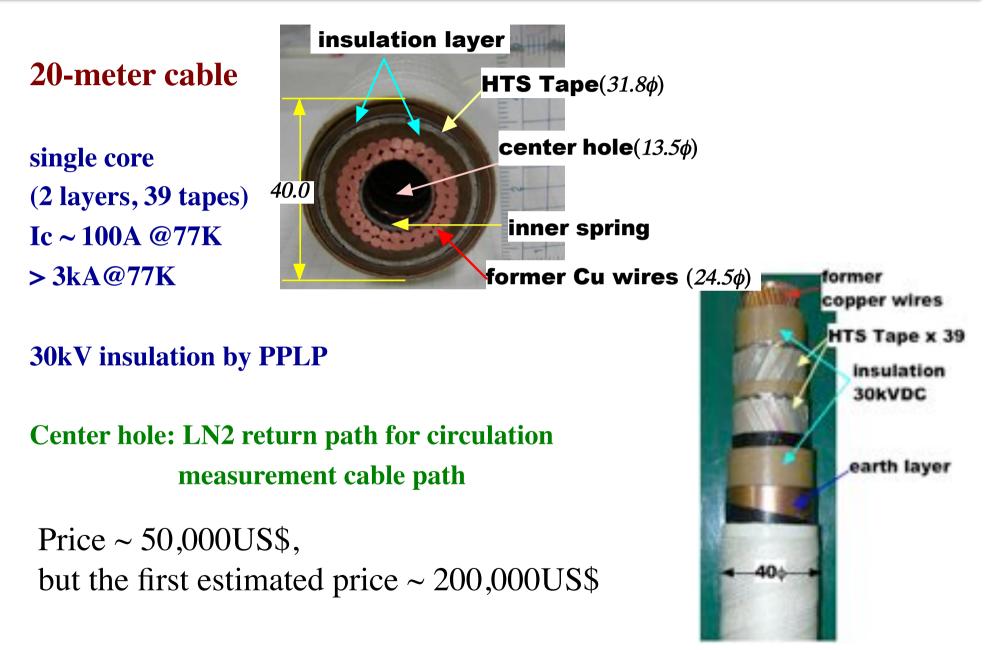
current > 2.5 kA voltage > 20 kV length ~ 20 m Sumitomo Bi-2223 cable

coolant; LN<sub>2</sub> equipped with pump and cryogenic cooler 72 K - 77 K

Measurement system ~ 500 CH by LabView

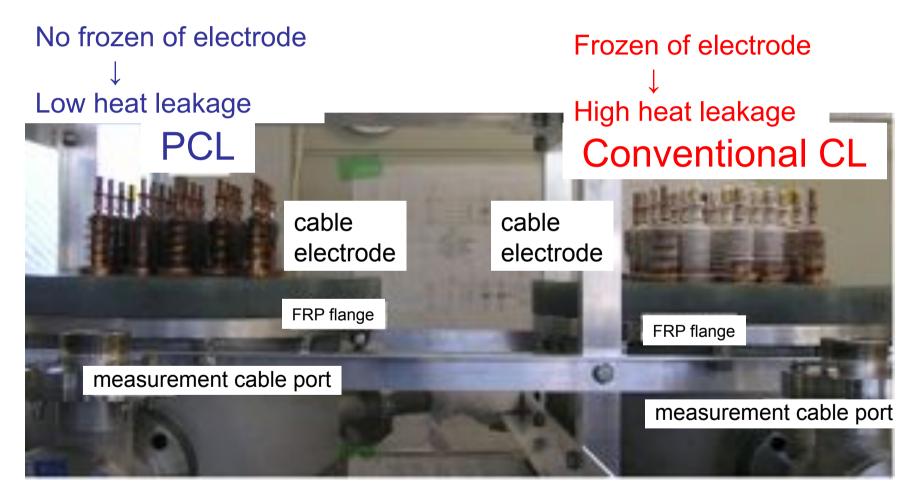
#### **First Experiment of HTS DC Cable System in the World**

### **Structure of 20-meter Cable**



Made by Sumitomo

### **Results of PCL@20m cable**



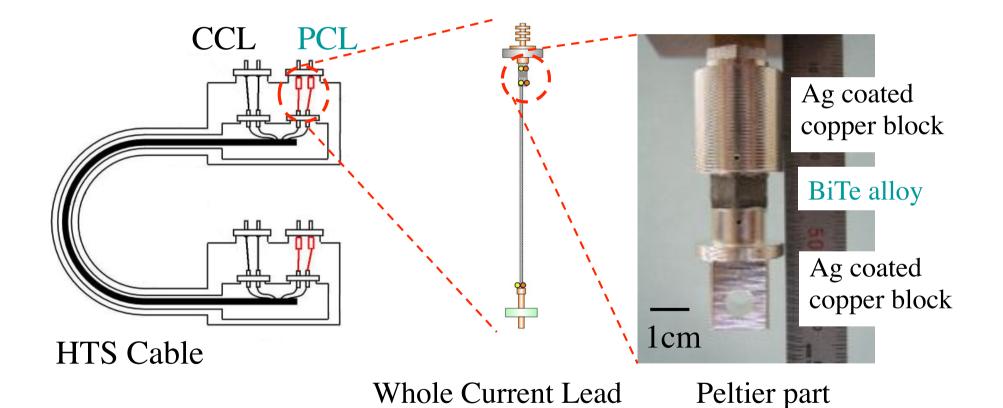
S. Yamaguchi et al, "Research activities of DC Superconducting Power Transmission Line in Chubu University ", J. Physics: Conference Series, **97**(2008)012290.

# **Results of PCL@20m cable**

IASS Workshop @2011/05/13, Potsdam

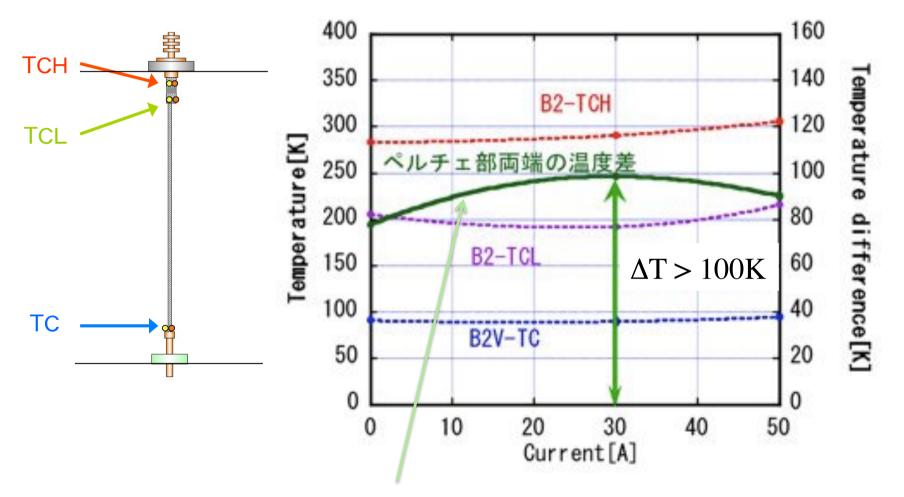
CASER-1

#### Reduction of Heat Leak from Current Lead



# **Results of PCL@20m cable**

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Temp. difference is larger than 100 K @current of 30A

# **Performance of PCL**

#### Heat Leakages of PCL and Conventional current lead (CCL)

	f = 0	f = 1	
CCL	42.5	23.3	II 4 I 1
PCL	26.7	18.6	Heat Leak unit (W/k

#### **Energy balance of PCL (for Bi-Te alloys)**

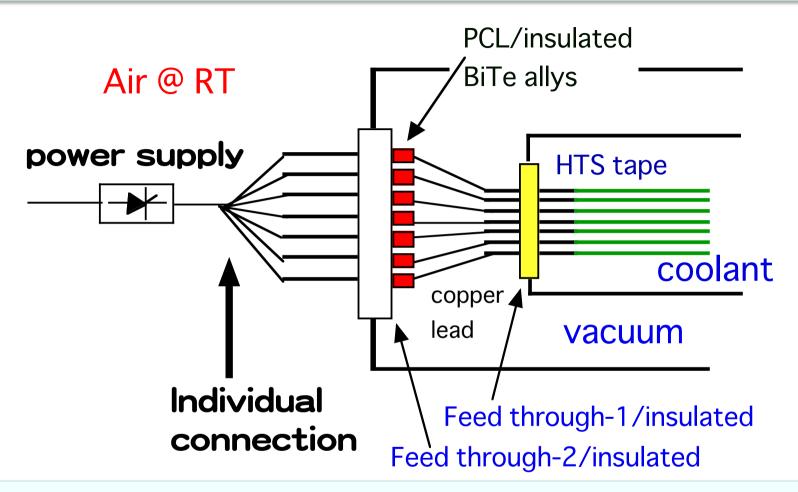
For 100A current lead Difference of Heat Leakage between CCL – PCL (f = 0) 4.25 – 2.67 = 1.58 [W] If we use refrigerator of COP = 0.067 (Sterling cycle) Saving Power = 1.58/0.067 = 23.6 [W]

Additional Loss of PCL Voltage of PCL =  $52mV \rightarrow 52mV \times 100A = 5.2$  [W]

S. Yamaguchi et al, "Peltier current lead experiments and their applications for superconducting magnets", RSI, **41**(2004)207.

► advanced PCL: gas-cooled PCL & Multi-stage current lead

# **Terminal connection@20m cable**

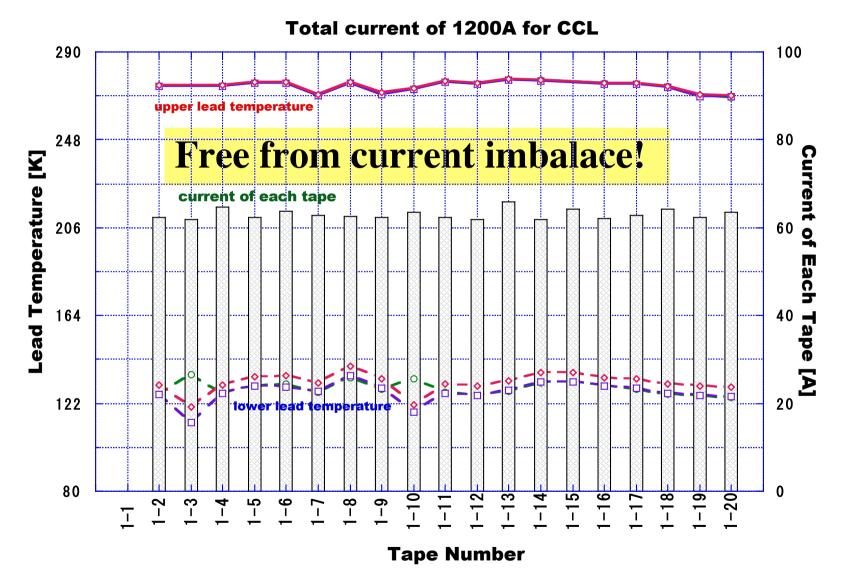


Important Structure to avoid the current imbalance of HTS tape for longer cable (> several km)

N. Koizumi et al, "Experimental results on instability caused by non-uniform current distribution in the 30 kA NbTi demopoloidal cpo; )DPC-U) conductor", Cryogenics, **34**(1994)155-162.

S. Yamaguchi et al, "A small-scale experiment demonstrating the current lead resistance method of preventing a current imbalance", Cryogenics, **38**(1998)875-880.

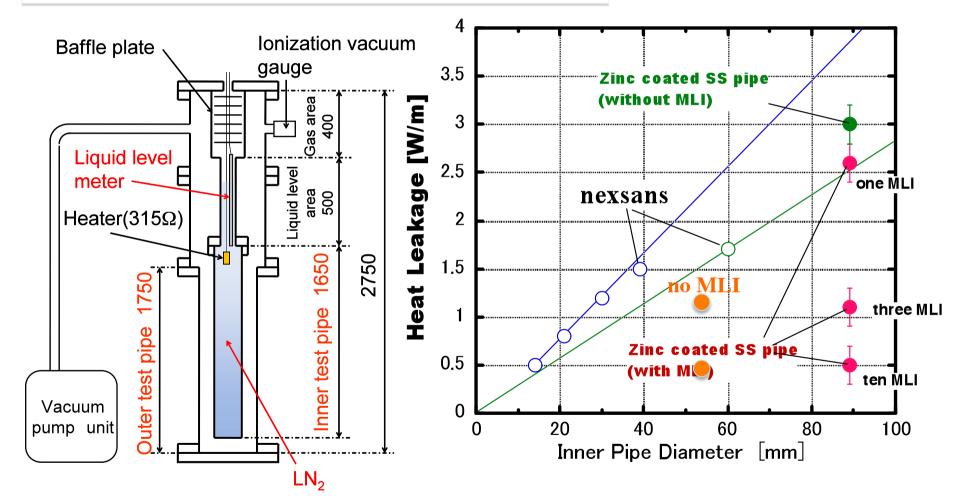
### **Current of each HTS Tape@20m cable**



S. Yamaguchi et al, "Research activities of DC Superconducting Power Transmission Line in Chubu University ", J. Physics: Conference Series, **97**(2008)012290.

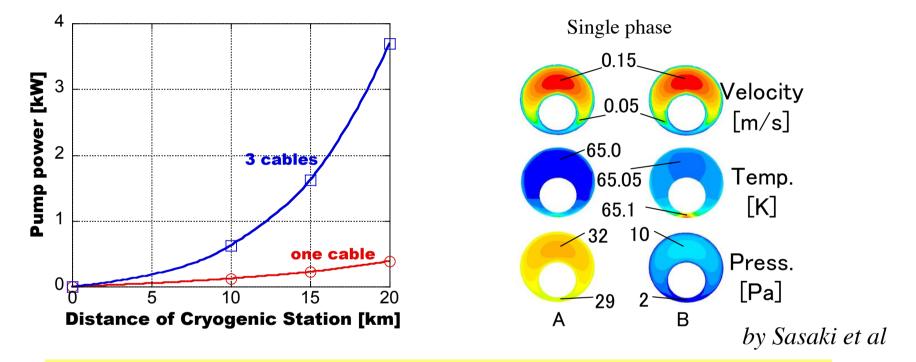
### Heat leak of Cryo-pipe@Test Stand

### Low Heat Leakage even for Fewer MLI Use low cost Iron pipe



M. Hamabe et al, "Measurement on Thermally-Isolated Double-Pipe for DC Superconducting Power Transmission", Advances in Cryogenic Engineering, **53A**(2008)168-173.



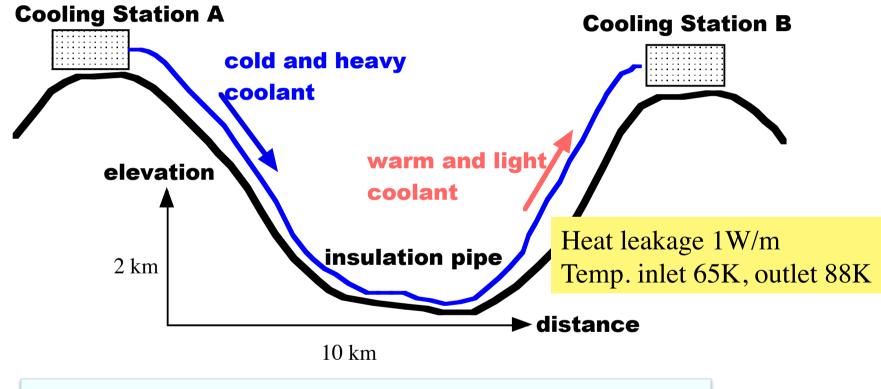


DC pressure drop (**one cable**) << AC (10 times higher, **three cables**), But, in the actual design (**pressure drop > 100 times**)

Experiment is need in long cable!  $\Rightarrow$  200 meter cable

A. Sasaki et al, "Cryogenic Fluid Dynamics for DC Superconducting Power Transmission Line", *IEEE Trans. Appl. Supercond.* **17** (2007) 1748-1751.

# How to reduce pump power, Use Siphon!



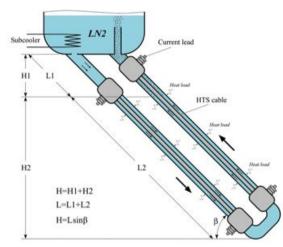
### Analysis of experimental data should be included, $\Rightarrow$ 200-meter cable experiment

Y. Ivanov et al, "A compact cooling system for HTS power cable based on thermal siphon for circulation of LN2", *Adv. Cryogenic Eng.*, **55** (2010) 865-870.

# **LN<sub>2</sub> circulation System**

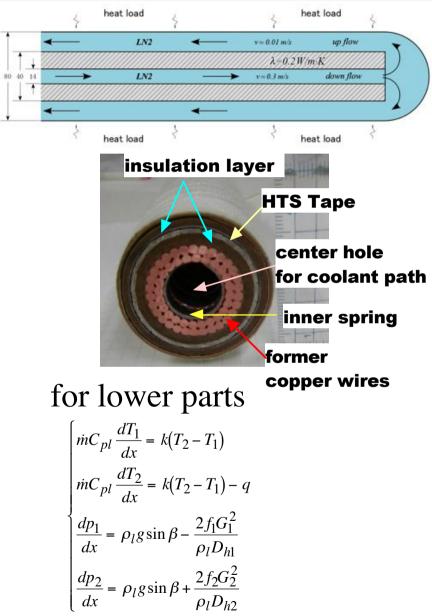
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#### **Model and Equations**



#### for upper parts

$$\begin{split} \dot{m}C_{pl} \frac{dT_{1}}{dx} &= k(T_{2} - T_{1}) \\ \dot{m}\left[(1 - \chi)C_{pl} + \chi C_{pg}\right] \frac{dT_{2}}{dx} + r\dot{m}\frac{d\chi}{dx} = k(T_{2} - T_{1}) - q \\ \frac{dp_{1}}{dx} &= \rho_{l}g\sin\beta - \frac{2f_{1}G_{1}^{2}}{\rho_{l}D_{h1}} \\ \frac{dp_{2}}{dx} &= \left(\frac{\chi}{\rho_{g}} + \frac{1 - \chi}{\rho_{l}}\right)^{-1}g\sin\beta + \frac{2f_{2}G_{2}^{2}}{\rho_{l}D_{h2}}\frac{1 + (\rho_{l}/\rho_{g} - 1)\chi}{\left[1 + (\mu_{l}/\mu_{g} - 1)\chi\right]^{0.25}} \\ T_{2} &= T_{sat}(p_{2}) \end{split}$$



Y. Ivanov et al, "A compact cooling system for HTS power cable based on thermal siphon for circulation of LN2", *Adv. Cryogenic Eng.*, **55** (2010) 865-870.

# **LN<sub>2</sub> circulation System**

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#### **Calculation Results**

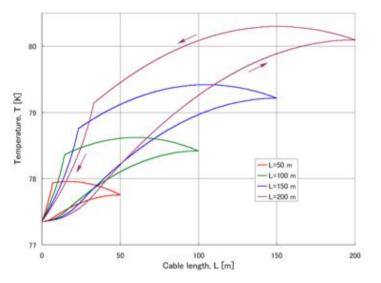


Fig.3 Temperature profiles for 50, 100, 150 and 200 m cables  $(sin\beta = 0.2)$ 

# It is effective for circulation to use Thermal siphon!

Y. Ivanov et al, "A compact cooling system for HTS power cable based on thermal siphon for circulation of LN2", *Adv. Cryogenic Eng.*, **55** (2010) 865-870.

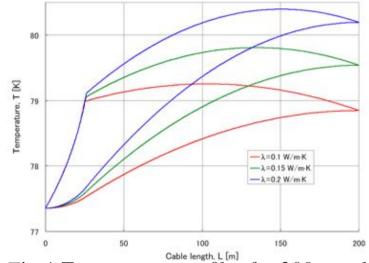


Fig.4 Temperature profiles for 200 m cable  $(sin\beta=0.25)$  as a function of heat conductivity of electrical insulator

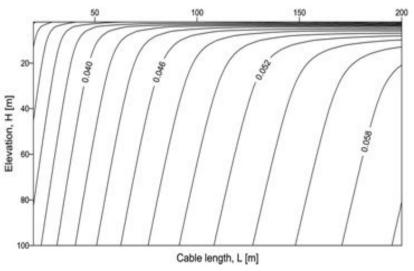
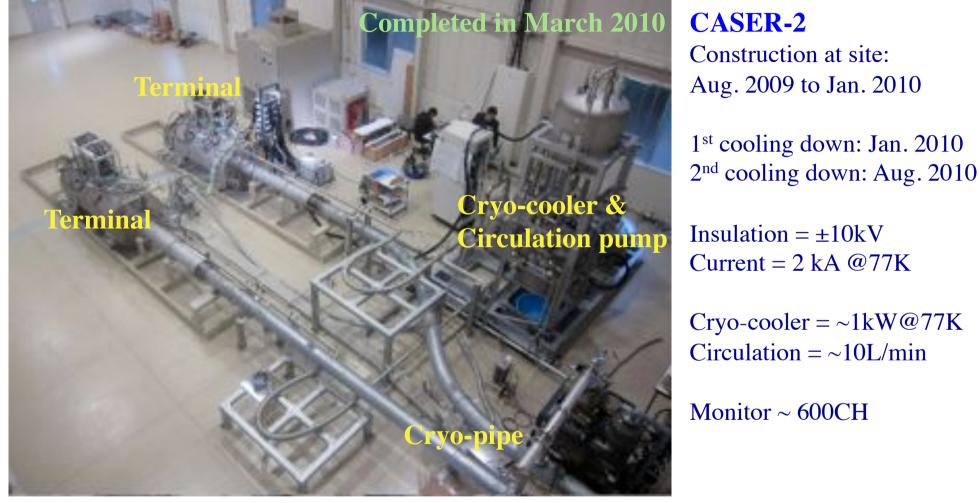


Fig.5 Mass flow [kg/s] versus cable length and elevation

#### **200-meter Cable Test Facility**

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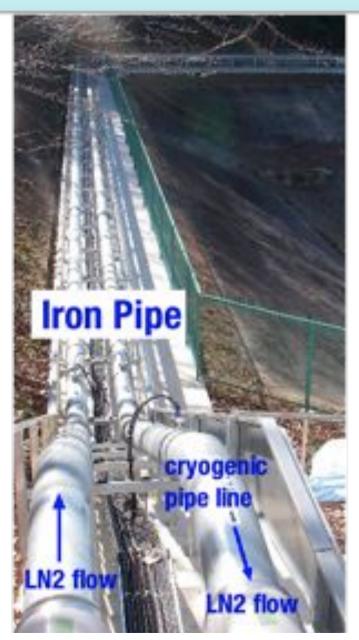


S. Yamaguchi et al, "**DESIGN and CONSTRUCTION of 200-meter HTS DC Power Cable Test Facility in Chubu University**", CEC-23/ICMC 2010, Poland July 2010.

Total budget ~ 5MUS\$(included labor cost of researchers)

### **Design of Cryogenic Pipe**

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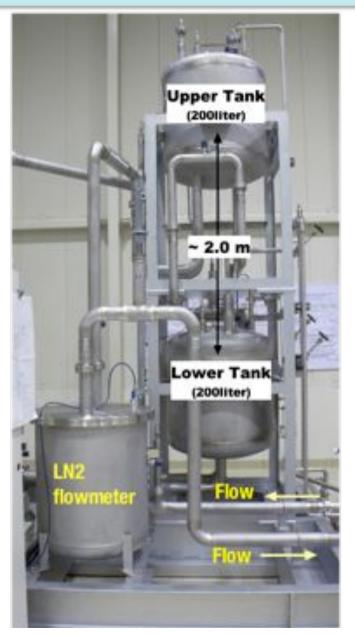
**20-meter cable experiment** 

200-meter cable experiment Iron Straight Pipe for outer pipe SS pipe for inner pipe

S. Yamaguchi et al, "**DESIGN and CONSTRUCTION of 200-meter HTS DC Power Cable Test Facility in Chubu University**", CEC-23/ICMC 2010, Poland July 2010.

### **Cryo-cooler & Cryogenic Tanks**

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Cryo-cooler ~ 1kW@77K operation temperature = 72K - 82K

Low pressure drop for circulation, Not connect the pump directly

Upper tank & lower tank system 1) pump does always not work 2) slush N2 experiment available **Operation**  $\Delta P = 10kPa - 30 kPa$ 

S. Yamaguchi et al, "**DESIGN and CONSTRUCTION of 200-meter HTS DC Power Cable Test Facility in Chubu University**", CEC-23/ICMC 2010, Poland July 2010.

### **Small diameter cable**

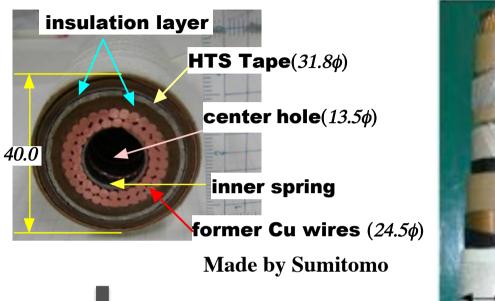
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former

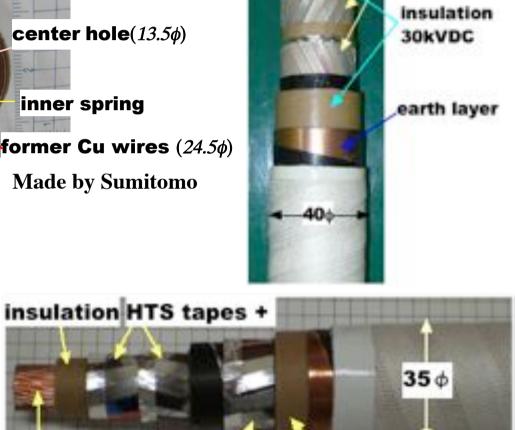
copper wires

HTS Tape x 39

20-meter cable Single wire (2 layers, 39 tapes) 30kV insulation >3 kA @78K



Former



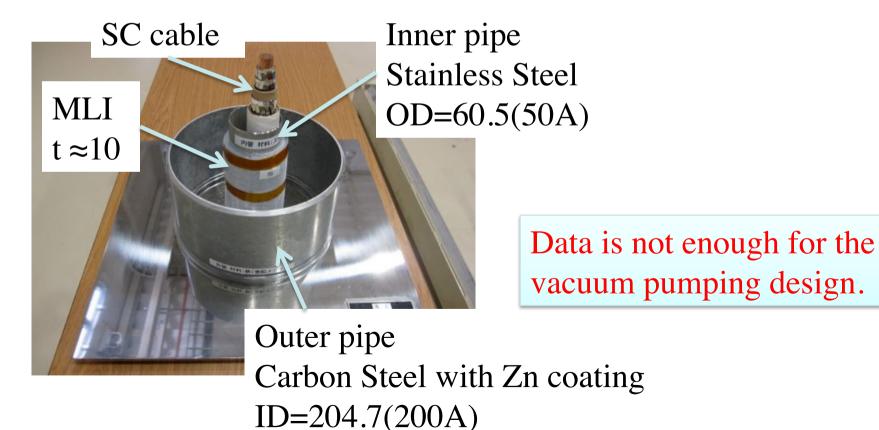
HTS tapes - insulation

200-meter cable = co-axial Inner (2 layers) = 23 tapes Outer (1 layer) = 16 tapes Insulation = ±10kV Current = 2 kA @78K Copper former = 14 $\phi$ 

### **Structure of Cryogenic Pipe & Cable**

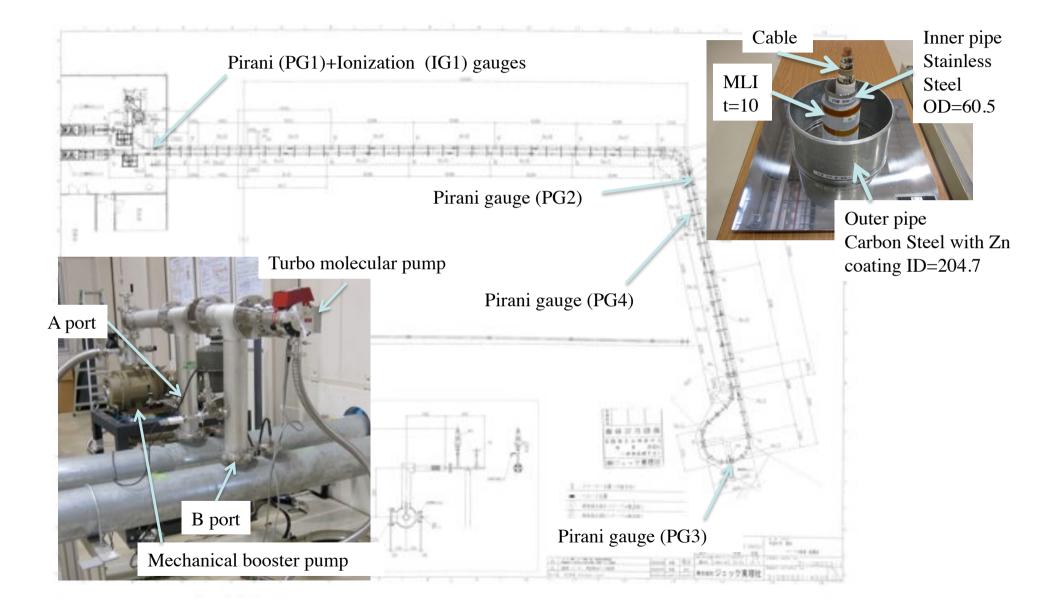
Vacuum pumping is a key subject for long pipe,
1<sup>st</sup> Priority of the Design is wider space for vacuum pumping.
→ H. Watanabe et al, SAP-9, ISS2010

- H. Watanabe et al, 22A-PS-3, ICEC23/ICMC2010
- H. Watanabe et al, "超伝導送電用長距離断熱配管の真空排気", 1P-p16, CE Japan

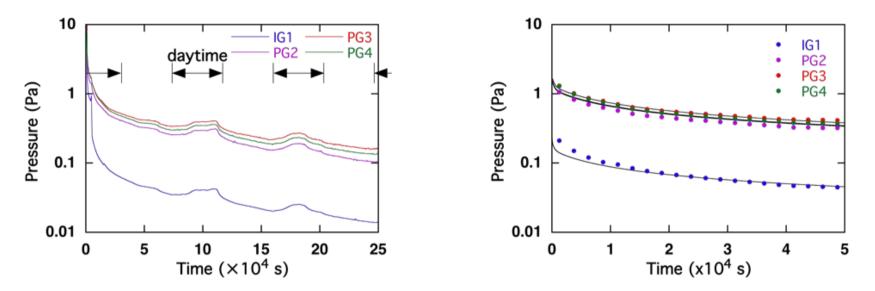


### The vacuum system for CASER2

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### Evacuation for vacuum insulation



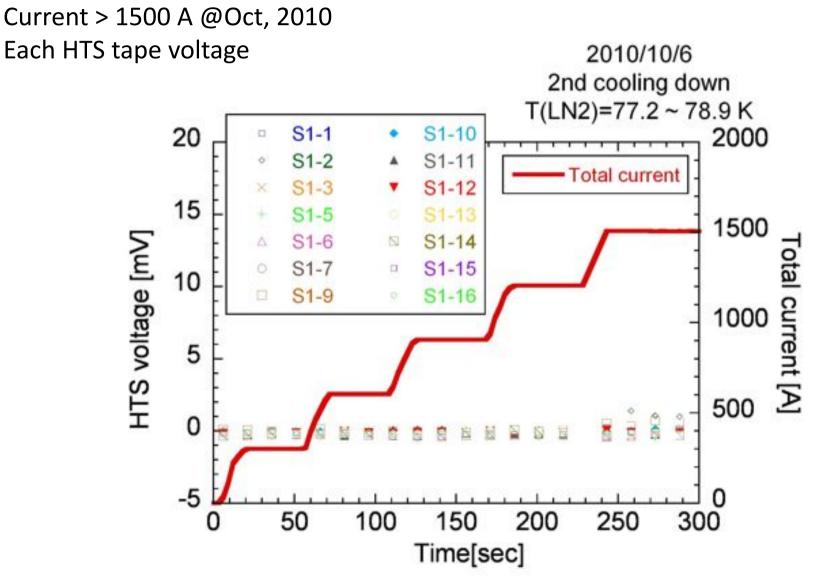
Evacuation time obtained by simulations with different conditions

Vacuum degree	Present situation		Out-gasing rate 20% reduction	Conductance 50% increase
0.1 Pa	9days	10days	6days	4days
0.05 Pa	37days	41days	23days	18days

A 200m cryogenic pipe is evacuated at the middle with a TMP of 260 l/s. The conductance of  $3001 \cdot \text{m/s}$  and the outgassing rate of  $6.8t^{-0.5}\text{Pa} \cdot 1/(\text{s} \cdot \text{m}^2)$  are supposed to obtain the result "present situation".

### Excitation of DC Cable

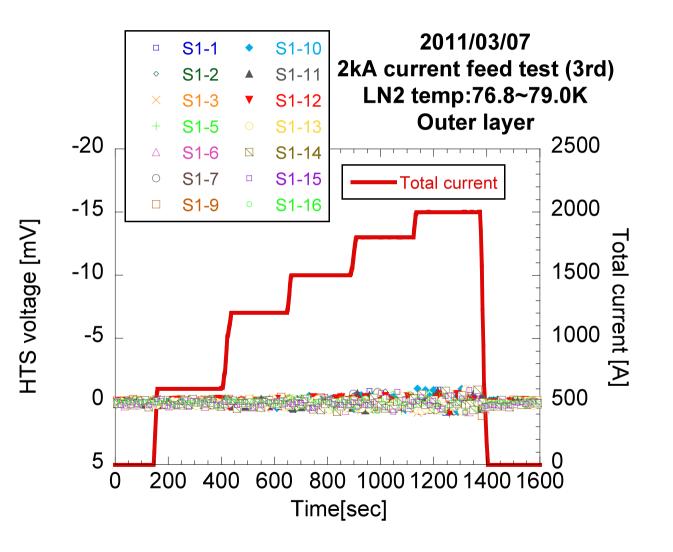
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Outer layer of cable.

# Current feeding test up to 2 kA

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We adjusted the length of each power cable between DC power supply and HTS tape by several m  $\Omega$ 

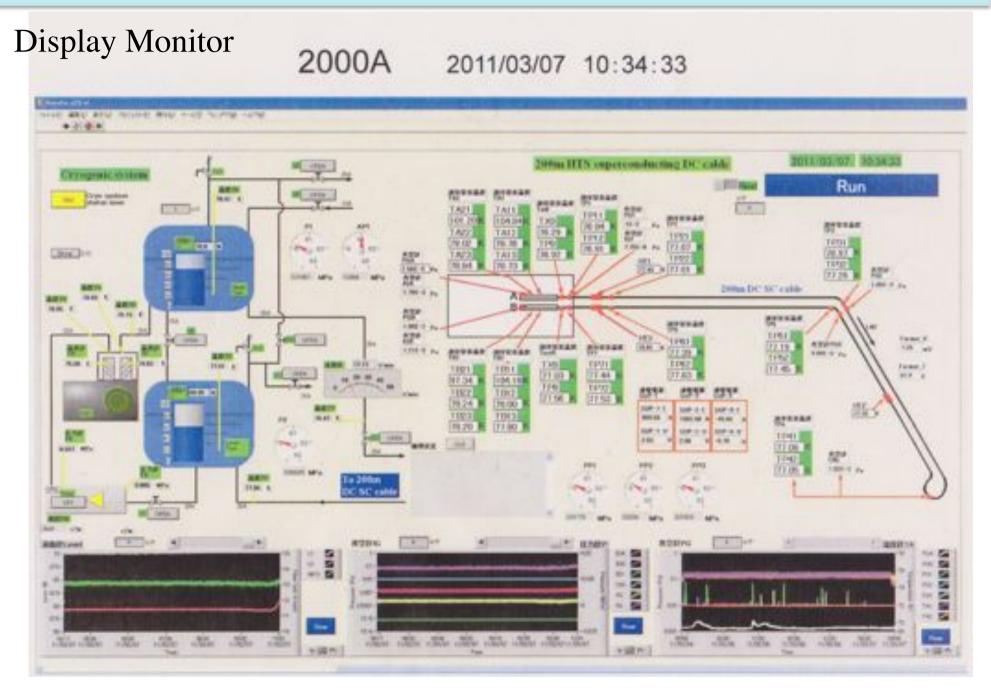


between HTS tapes can be suppressed

Operation up to 2 kA has succeeded.

# Current feeding test up to 2 kA

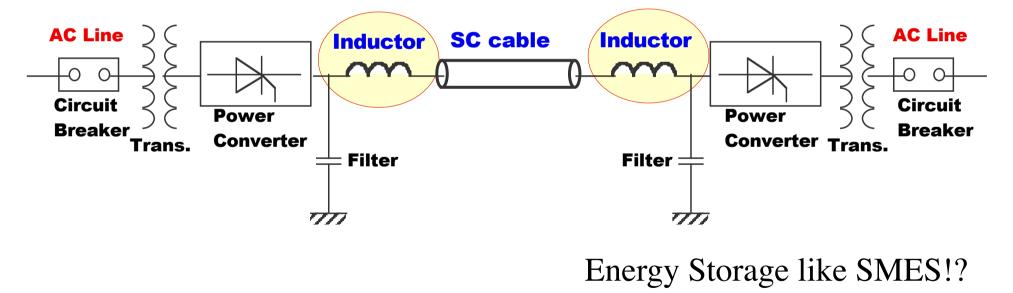
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DC Transmission Line needs Larger Inductors to reduce the ripple of current & short circuit current.

System of Iron pipe + Single core cable



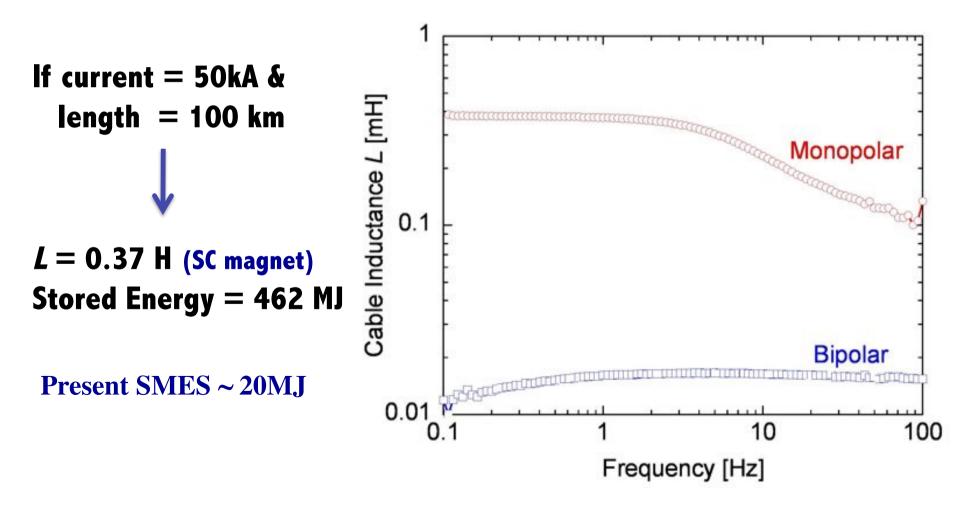
S. Yamaguchi et al, "Iron-steel cryogenic pipe for DC superconducting power transmission line", ASC2010, Washington DC, USA August 2010.

Inductance of DC Cable

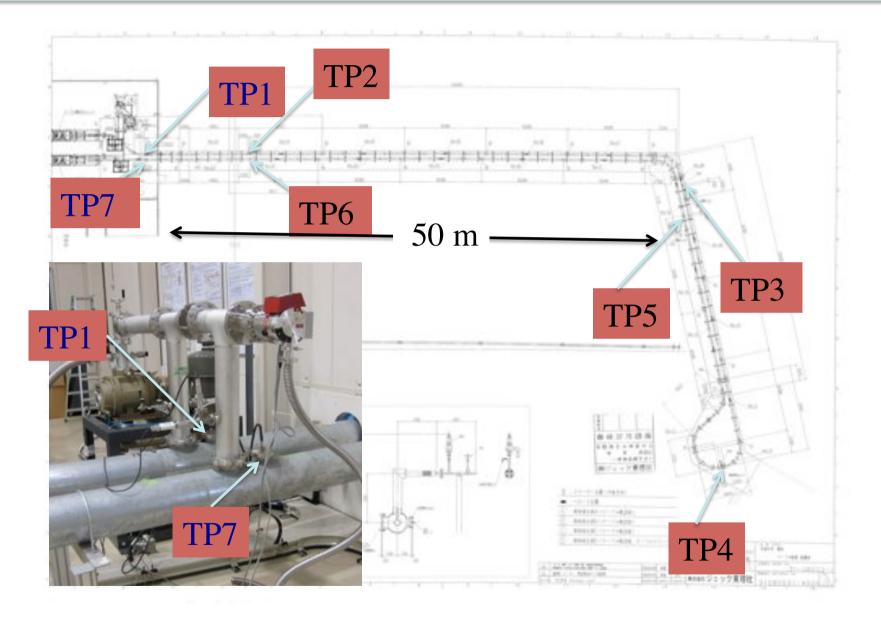
### **Energy Storage by Grid**

L = 0.37 mH for 100m cable measured at the current of 400A, Higher inductance depends on Iron material of outer pipe.

→ M. Hamabe et al, SAP-10, ISS2010

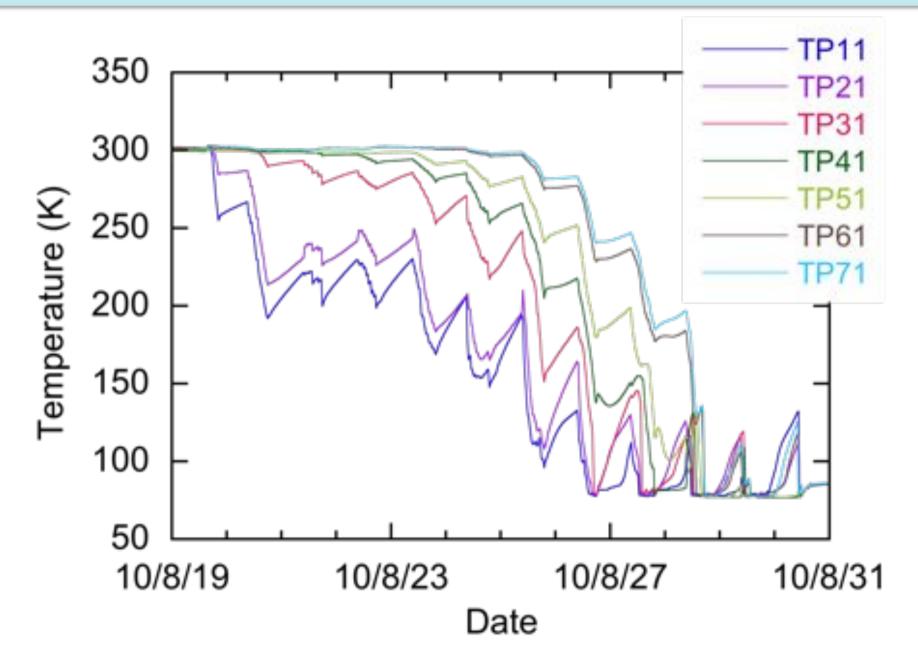


#### **Thermometer positions**



### 2<sup>nd</sup> Cooling Down

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### **Thermal expansion & Support Structure**

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#### nexans



CRYOFLEX( flexible, vacuum insulated cryogenic envelopes consist of two concentric, corrugated tubes. The tubes, together with their associated terminations and hardware, are assembled, leak tested and evacuated at the factory.

#### Design:

Helically corrugated and longitudinally welded stainless steel tubes Diameter range from 10 to 300 mmrom 10 to 300

http://www.nexans.com/eservice/Navigate.nx?navigationId=142392

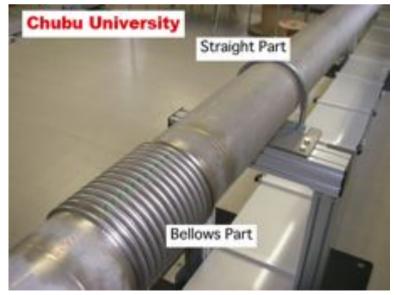
#### Chubu Univ. & LHC/CERN

#### **Straight & Bellows Pipes**

- 1) High Strength
- 2) Cheap
- **3)** Low pressure drop
- 4) the other reasons

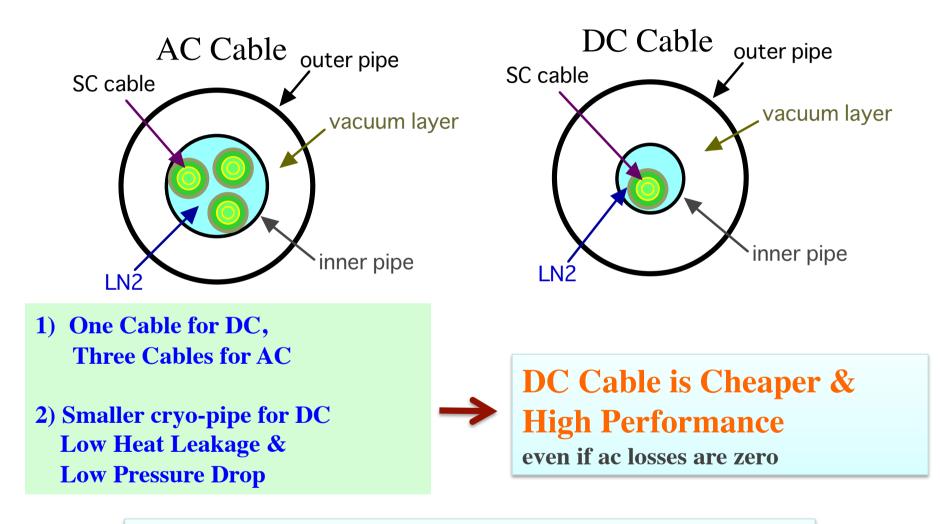
#### How to absorb HTS tape thermal shrinkage?

#### Water pipe structure



# **Difference of DC & AC Cable**

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# We should confirm experimentally!

# Lying Cable Method

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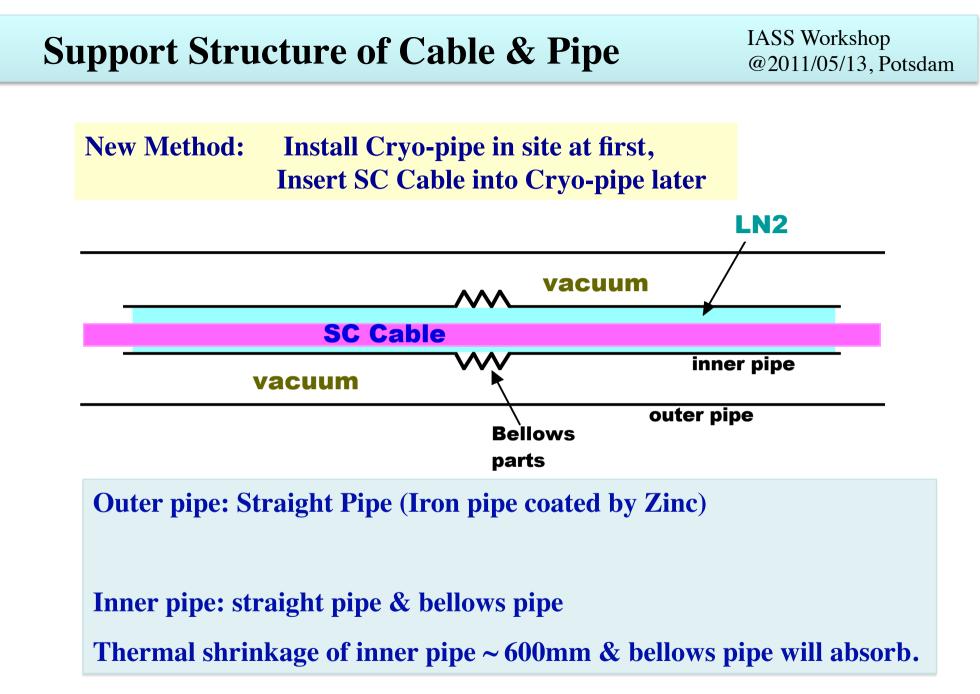
#### Previous Method: compose Cable & cryo-pipes in factory at first, Install Cable with cryo-pipe in site Merit: Easy installation for short distance



Sumitomo et al

▲三心一張型超電導ケーブル

However, many connection parts for long distance *High Cost of connection + Cabble Accidents will increase!* 

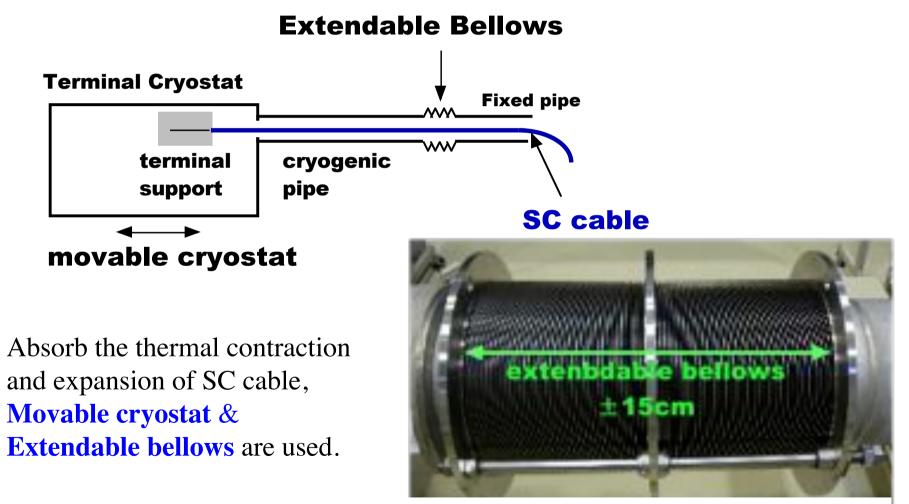


S. Yamaguchi et al, "**DESIGN and CONSTRUCTION of 200-meter HTS DC Power Cable Test Facility in Chubu University**", CEC-23/ICMC 2010, Poland July 2010.

# **Cable support at Terminal Cryostat**

### **Reduction of thermal stress of HTS tape is important!**

M. Sugano, K. Shikimachi, N. Hirano and S. Nagaya, Supercond. Sci. Technol., 23(2010)085013.

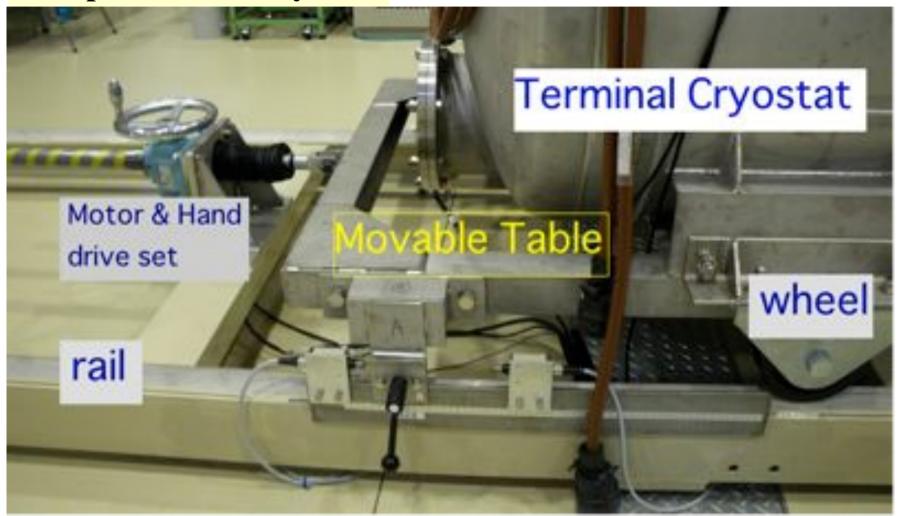


S. Yamaguchi et al, "**DESIGN and CONSTRUCTION of 200-meter HTS DC Power Cable Test Facility in Chubu University**", CEC-23/ICMC 2010, Poland July 2010.

### **Movable Cryostat**

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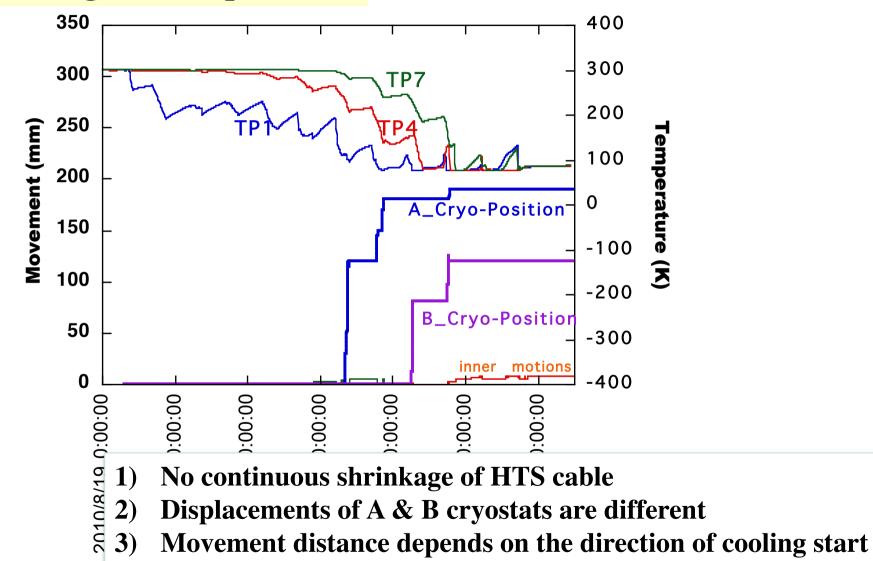
#### **Computer control system**



S. Yamaguchi et al, "Experiment of 200-meter Superconducting DC cable system in Chubu University", accepted in publication in *Physica C*.

IASS Workshop @2011/05/13, Potsdam

#### 2<sup>nd</sup> cooling down experiment



S. Yamaguchi et al, "Experiment of 200-meter Superconducting DC cable system in Chubu University", accepted in publication in *Physica C*.

## **Summary of Cryostat Motions**

#### Cryostat positions of 1<sup>st</sup>, 2<sup>nd</sup> and 3<sup>rd</sup> Experiments

	Cryostat A [mm]	Cryostat B [mm]
After Construction	0.0	0.0
1 <sup>st</sup> Cooling Down	-163	-299
1 <sup>st</sup> Warming up	+28	-181
2 <sup>nd</sup> Cooling Down	-162	-294
2 <sup>nd</sup> Warming up	+7	-100
3 <sup>rd</sup> Cooling Down	-207	-238
3 <sup>rd</sup> Warming up	+6	-99

Since the cables are not fixed to the cryostat,

- 1) These displacements are not real length of Cables
- 2) Movements are not constant for cooling down & temperature rise

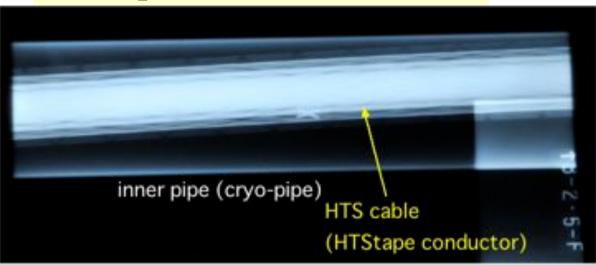
X-ray Photos

S. Yamaguchi et al, "Experiment of 200-meter Superconducting DC cable system in Chubu University", accepted in publication in *Physica C*.

## X-ray photos of cryo-pipe & cable

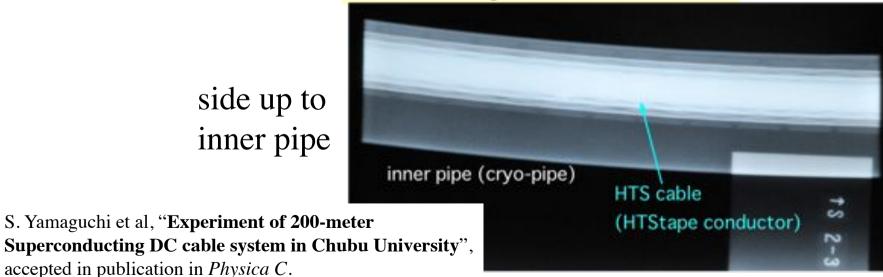
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#### 1<sup>st</sup> temperature rise (~@300K)



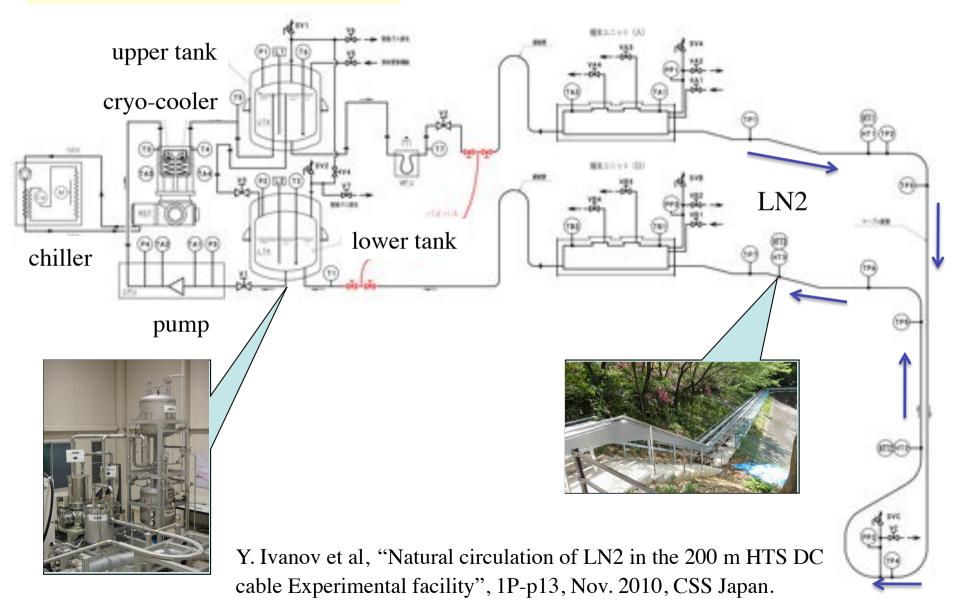
helically twisted way

#### 2<sup>nd</sup> cooling down (~@77K)



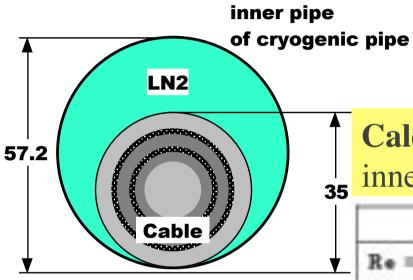
## **Circulation of LN2**

#### **Setup of circulation path**



## **Cryogenic Circulation Design**

#### **Configuration of inner pipe & cable**

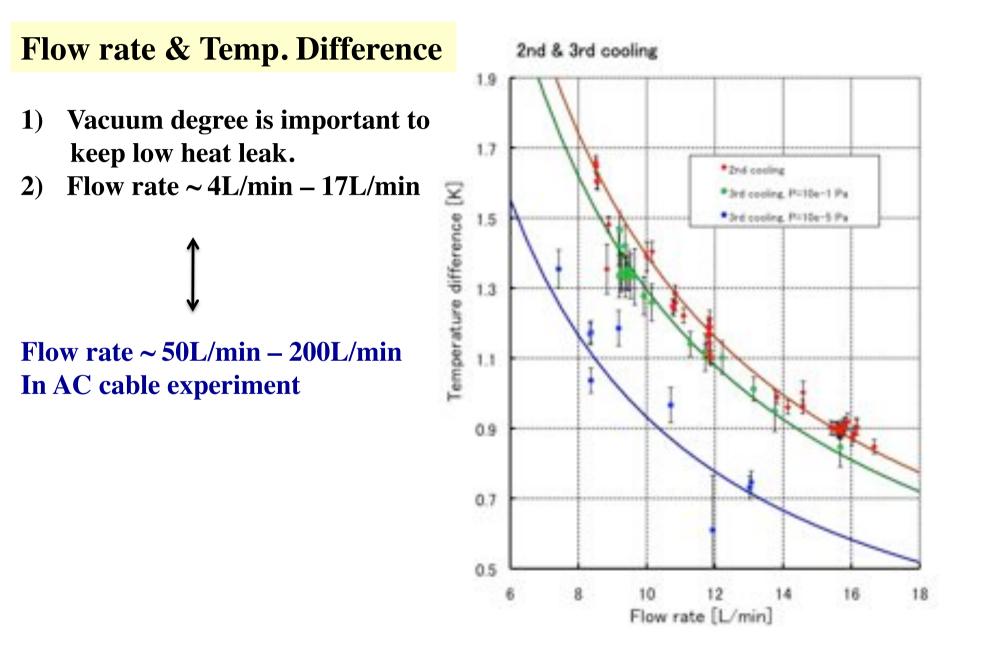


### Calculation

inner straight SS pipe with bellows pipe (<5%)</li>

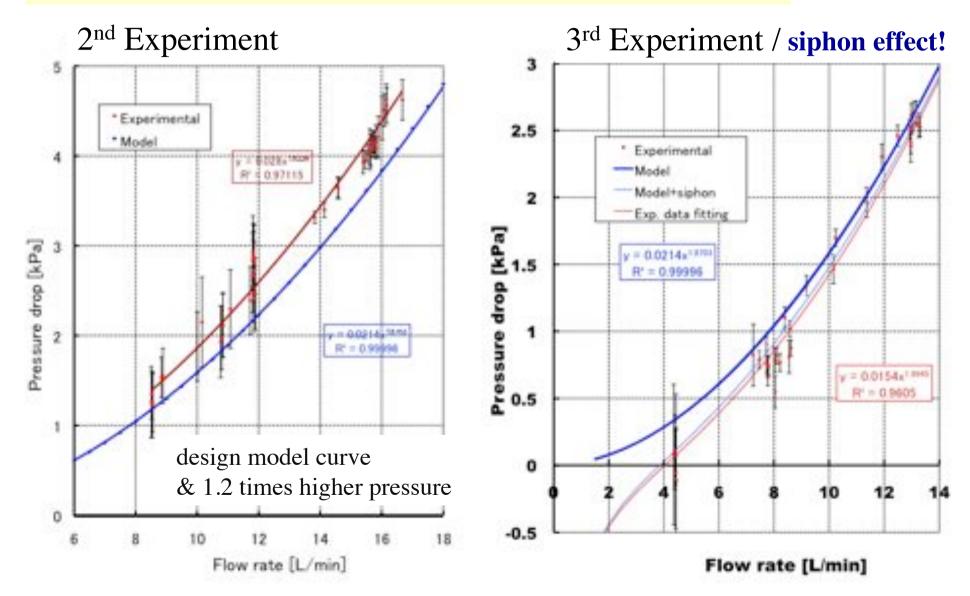
Formula		
$Re \equiv \rho v D_k / \mu$	$\Delta P = 2 f \rho v^2 L / D_h$	
Re: Reynolds number	Δ P: pressure drop [Pa]	
p: density [kg/m <sup>8</sup> ]	L: length of pipe [m]	
v: flow velocity [m/s]	12 2525	
D <sub>k</sub> : hydraulic diameter [m]		
(for circular pipe, D <sub>b</sub> =D <sub>2</sub> -D <sub>1</sub> )	$\Delta T = q_w L/v A_{kp} C_p$	
p viscosity [Pa s]	ΔT: temp. difference [K]	
$f = 0.0791/Re^{0.25}$ (Re>2000)	q. heat leak [W/m]	
f pipe friction factor	Ah: cross section [m <sup>2</sup> ]	
	C, specific heat [J/(kg K)]	

## **Experimental Result of LN2 Circulation**



### **Experimental Result of LN2 Circulation**

#### Pressure Drop & Flow rate in 2<sup>nd</sup> & 3<sup>rd</sup> Experiments



## **Estimation for Long LN2 Circulation**

Pressure drop = 
$$L^{2.75} \sim \underline{L}^3$$

Distance :	200 m →	$2 \text{ km} \rightarrow 20 \text{ km}$
$\Delta T$ :	1.5 K →	1.5 K → 1.5 K
Pressure :	1.5kPa →	1.5MPa → 1.5GPa
Flow Rate:	10 L/mim →	100 L/min → 1000 L/min

 $\Delta T \rightarrow 5 \text{ K} (70 \text{ K} \rightarrow 75 \text{ K}) \text{ for } 2 \text{ km}$ Flow rate  $\rightarrow 30 \text{ L/min}$ 

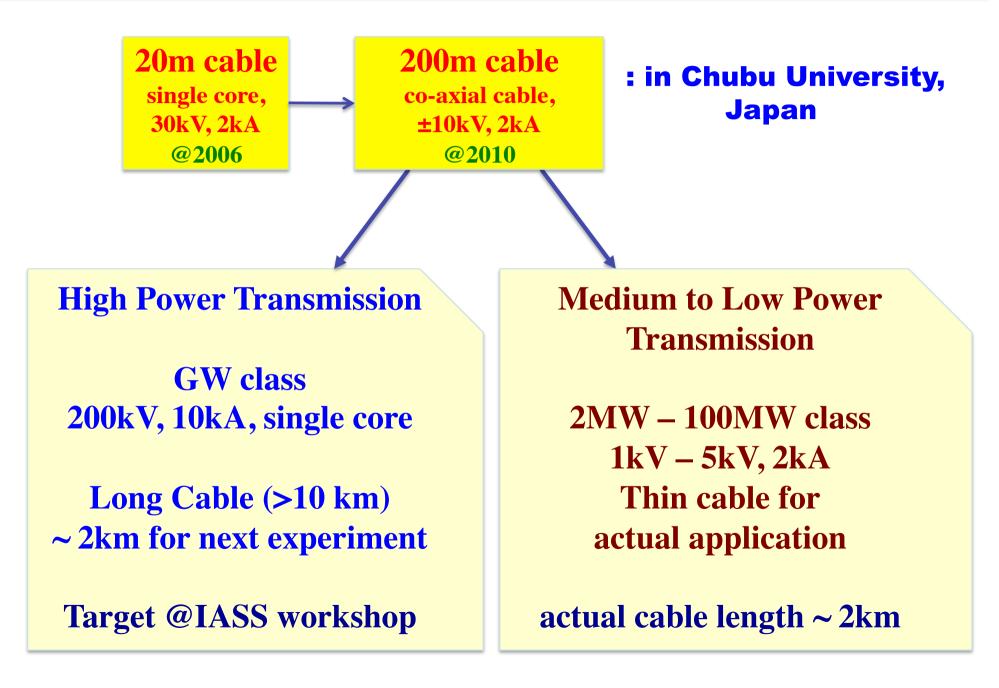
Pressure  $\rightarrow$  135 kPa

If heat leak will be half, the flow rate is 15 L/min & the pressure drop is 33.8 kPa

## Available in the Present Instruments till 2 km!

#### **New Test Bench for Heat Leakage** @2011/05/13, Potsdam New test bench for accurate measurement Main loss is heat leak of cryo-pipe for long transmission LN2 level meter LN2 in Radiation shield and out GN2 out 1) To flow meter gas measurements in CU for various types of pipes. Improvement of SI is 2) needed. Measurement part 1500 300 of LN2 level **Collaboration with JFE steel.** ~3000 acuum LN2 Inner test pipe 565 Outer test pipe 10°

**IASS** Workshop



## Cable Design of DC200kV/±10kA/4GW

•Structure of cable: Single-core, coaxial, and mono-pole cable. SC tape is for main line and Cu tape is for return line

•DI-BSCCO (Ic=200A) is employed as superconducting tape .

•Electric insulation is based on the results of previous DC insulation test, not confirmed.

	Former	Parameter	CASE 1	CASE 2
	SC Layer	Former	φ14mm	φ35mm
	(Forward line)	SC layer (Forward line)	6 Layers / 70 SC tapes lc=12500A	3 Layers / 64 SC tapes Ic=12500A
	Copper Layer (Return line)	Insulator	PPLP∶t=17mm	PPLP: t=13mm
N Protecting Layer for Cable Core		Copper layer (Return line)	Copper tape	Copper tape
		Protecting layer	φ60mm	φ70mm

#### **Collaboration with Sumitomo**

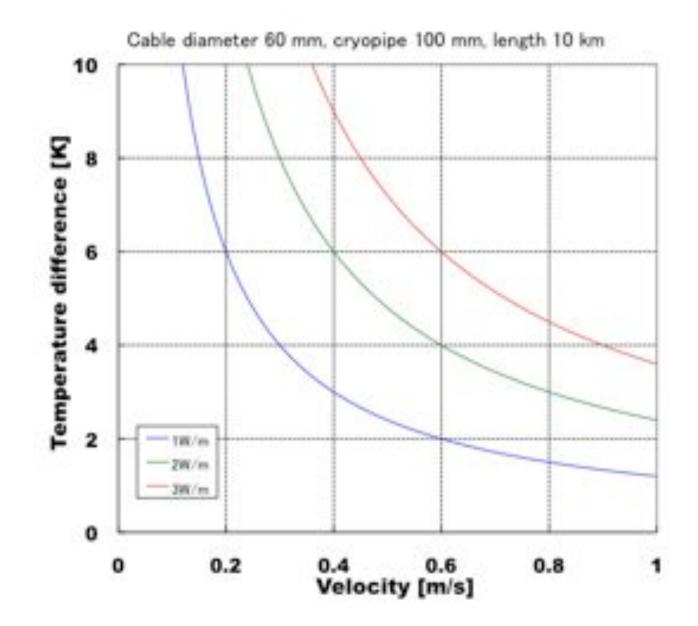
Price of Bi-2223 tape ~ 10 Yen/A • meter in 2011.

# **Test of SC-DC cable (proposal)**

IASS Workshop @2011/05/13, Potsdam

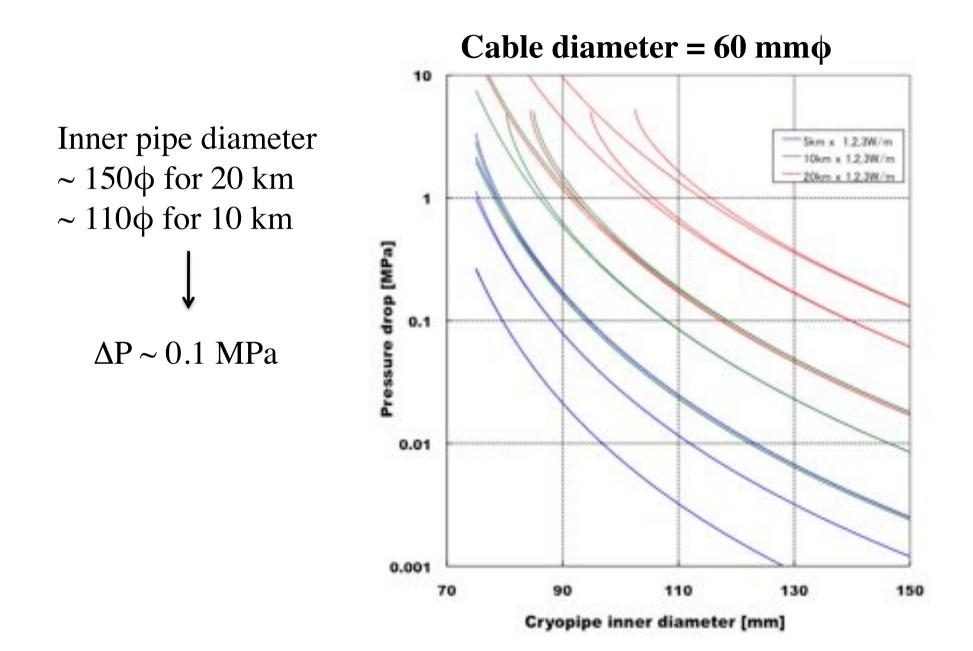
	Parameter	Target	Content and outline	Description	
Typical test	Bent test	30m Cable	Tested at the bent radius by IEC standard	Ic degradation is not observed.	CIGRE
	Load cycle test		8 hours operation, 16 hours non-operation by 20 cycles First 10 cycles: 1.8U0/Last 10cycles: -1.8U0	Positive voltage is sufficient for monopole cable.	CIGRE
	Polarity switching test		+-1.4U0, reversed at every 4 hours for 10 days	Not necessary for monopole cable	CIGRE
	Impulse withstand	accessaries	-U0+ positive switching surge, 10 times +U0+ negative switching surge, 10 times		CIGRE
	voltage test		-U0+ positive lightning impulse, 10 times +U0+ negative lightning impulse, 10 times		
	Ic test		Similar to specified value		SC
	Heatleak of cryopipe		Similar to specified value		SC
Droschinmont	High voltage test	Total length	1.8U0, 15 minutes	Total length test is hard for SC cable and sample test is advisasble.	CIGRE
	Conductor resistance	Sample	Similar to specified value	Ic test sbstitutes in SC cable	CIGRE
	Cable capacitance	Sample	Similar to specified value		CIGRE
	Ic test	Sample	Similar to specified value		SC
	Bent test	Sample	Tested at the bent radius by IEC standard.	Ic degradation is not observed	SC
Completion test	Voltage immpression	Total length	1.4U0, 15 minutes		CIGRE
	Ic test	Total length	Similar to specified value		SC
	Heatleak of cryopipe	Total length	Similar to specified value U0: r	ated voltage	SC

#### **Cooling for High Power and Long Cable**



## LN2 circulation for DC200kV/10kA cable

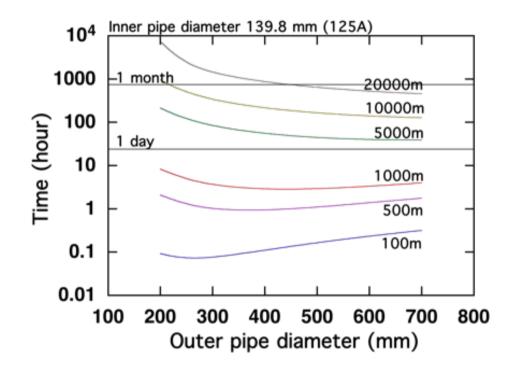
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#### Vacuum pumping for long cryogenic pipe

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# Evacuation time obtained by simulations for outer pipes with different diameters and lengths

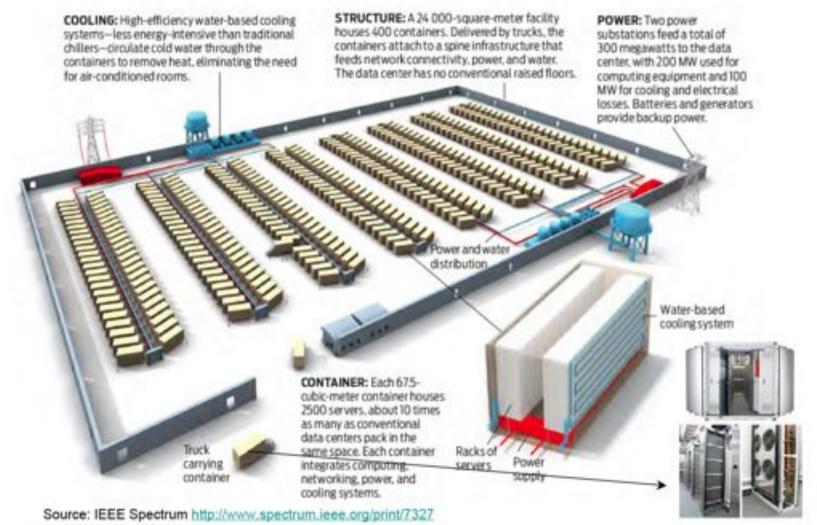


A cryogenic pipe is evacuated at the middle with a TMP of 100 l/s from 1 Pa. The out-gassing rate of  $2x10^{-5}t^{-0.28}$ Pa·l/(s·m<sup>2</sup>) is supposed. This improved out-gassing rate was obtained during the 3<sup>rd</sup> cooling down experiment.

#### **Diameter** ~ $600\phi$ for vacuum pumping.

## **Application for Data Center**

#### IASS Workshop @2011/05/13, Potsdam



and Distribution, Cambridge, MA, Feb. 25, 3000

# We must learn how to manage the DC SC transmission from Short Distance

# Comparison with CV cable



Electric Power = 40MW voltage = DC400V current = 100kA cable length = 250m

Resistivity  $= 0.02 \ \mu\Omega m$ Current density  $= 1 \text{A/mm}^2$ 

Number cable = 308 (325mm^2/cable)

Loss = 6.5 W/m for one cable

Total Loss =  $308 \times 2 \times 250 \times 6.5$ = 1.0 MW Loss of SC Cable

COP of Ref.	= 0.1 @70K
Terminal heat leak	= 25W/kA
Heat Leak of Cryo-pipe	= 1 W/m
cable length	= 250 m

Loss of terminal = 25 x100 x 4 x 10 = 100 kW

Loss of Cryo-pipe =  $1 \times 250 \times 10$ = 2.5 kWOthers = 20 kW

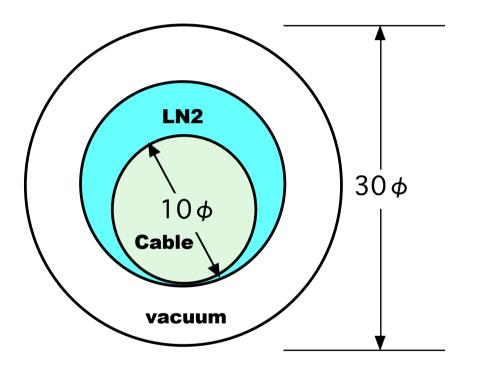
Total Loss =100 + 2.5 + 20 = 122.5 kW

Type of Terminal	Heat Leak	comments
copper lead	~50W/kA	Common use in the present time
Pelteir current lead (PCL)	~25W/kA	R&D phase for commercial use
Gas-cooled PCL	12 ~18W/kA	Start the experiment in CU
New current lead	5 ~ 10W/kA	Theoretical estimation based on the performance of the present commercial instruments

If heat leak of 5 - 10 W/kA is achieved in the terminal, we can find wide applications because several companies started to develop high COP refrigerator (COP ~ 0.1 @70K).

# Low voltage DC\_SC Cable

#### **Design Study for iDC, Electric Train, Steel Mill**



DC bi-pole cable : 400V ~ 1.5kV ~ 4kV 1.0kA ~ 2.0kA > 1MW

Cryo-pipe outer  $\sim 30\phi - 50\phi$ short distance

Transfer tube cost is higher than cable's!

Cheaper than copper wire? But lower losses. LN2 or LNG transfer tube is available! (heat leak < 0.5W/m)

# 200-meter cable experiment for 2.5 years construction & operation

```
Total budget ~ 5MUS$(included labor cost of researchers)

cable cost ~ 20% (included R&D in Sumitomo)

HTS cost ~ 6% (200US$/kAm)

Researcher ~ 20% (5 persons)

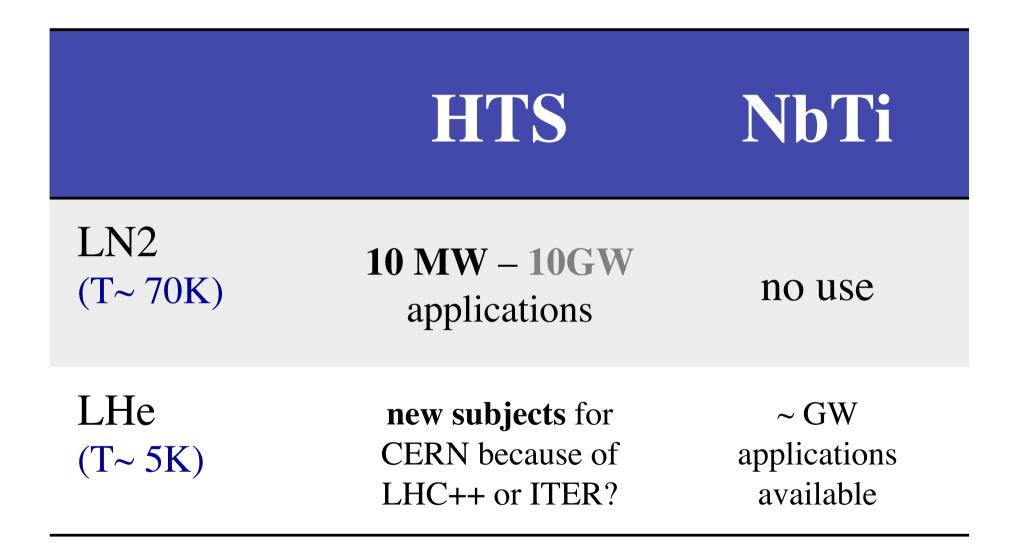
overhead ~ 5% for University
```

If we use HTS @6K, HTS cost is less than 10US\$/kAm. Is it cheap or not for NbTi wire?

```
NEDO target ~ 30US$/kAm @70K in Japan, therefore 3US$/kAm @6K?
```

Subject for discussion – 2 (application)

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# ICBM is Peace Keeper in Cold War

#### IASS Workshop @2011/05/13, Potsdam

Deterrent Theory: Intercontinental Ballistic Missile could keep Peace in cold war.

#### **Specifications and Performance**

Weight88,450 kgLength21.6 mDiameter2.34 mRangeOver 11,000 kmSpeed24,000 km/hr; 6.7 km/secCeiling805 kmThrow Weight3950 kg; PBV vAccuracy (CEP)100 m

 Warheads

#### Launch of Missile

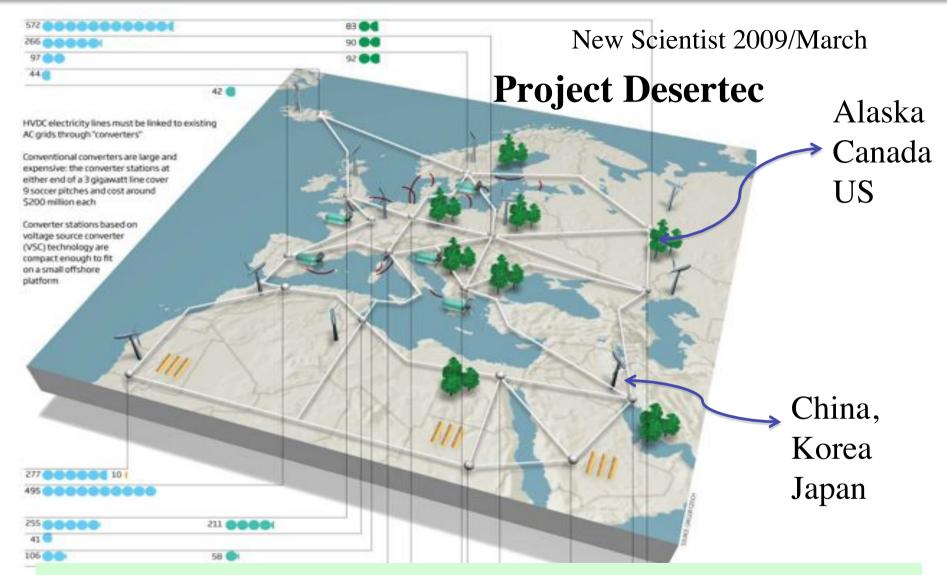


3950 kg; PBV weight 1365 kg; Net warhead load 2585 kg 100 m

#### Propulsion

First Stage Second Stage Third Stage Post-Boost Stage 2,200,000 KN thrust Thiokol solid fuel motor; Weight 49,000 kg Aero-jet General solid fuel motor; Weight 27,000 kg Hercules solid fuel motor; Weight 7,700 kg Rocket-dyne re-startable liquid fuel motor; storable hypergolic fuel

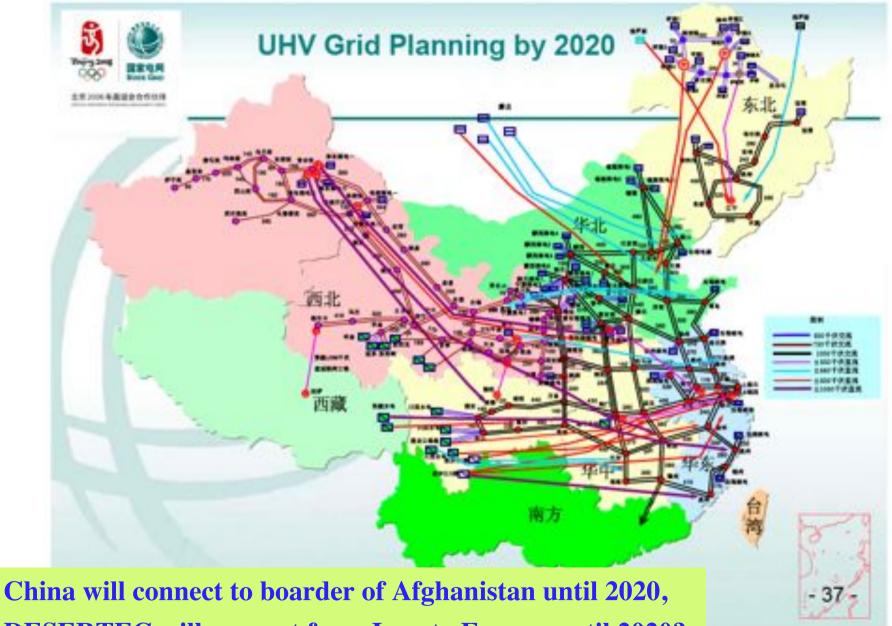
# A New Peace Keeper, DC\_SC Transmission [ASS Workshop @2011/05/13, Potsdam]



Neighbour Countries should keep a good relation to get Energy inspite of they do not like each other.

## **UHVDC in China**

#### IASS Workshop @2011/05/13, Potsdam



**DESERTEC** will connect from Iran to Europe until 2020?

#### A New Peace Keeper, DC\_SC Transmission <sup>IASS Workshop</sup> @2011/05/13, Potsdam

Now we have ~500 Nuclear Stations in the World, we will make ~2000 Nuclear Stations in 21<sup>st</sup> Century

Europe (mid night)  $\longrightarrow$  Japan (day time) Europe (day time)  $\leftarrow$  Japan (mid night)





And connect Energy from Desert. Can we get the budget from defense because of keeping peace?